CERTIFICATES OF COMPETENCY IN THE MERCHANT NAVY MARINE ENGINEER OFFICER

## EXAMINATIONS ADMINISTERED BY THE SCOTTISH QUALIFICATIONS AUTHORITY <br> ON BEHALF OF THE <br> MARITIME AND COASTGUARD AGENCY

## CHIEF ENGINEER REG.

APPLIED HEAT

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Attempt SIX questions only.

## All questions carry equal marks.

Marks for each part question are shown in brackets.

1. A perfect gas expands reversibly in a cylinder according to the law $\mathrm{pl}^{1.5}=$ constant and is then heated at constant volume.

The initial pressure and temperature are 90 bar and $1800^{\circ} \mathrm{C}$ respectively. The final pressure is 2 bar and the final volume is twenty times the initial volume.
(a) Sketch the processes on Pressure-Volume and Temperature-specific entropy diagrams.
(b) Calculate EACH of the following:
(i) the temperature after expansion;
(ii) the final temperature;
(iii) the net change in specific entropy.

Note: For the gas $R=0.287 \mathrm{~kJ} / \mathrm{kgK}$ and $\gamma=1.33$
2. A compression ignition engine working on the ideal dual combustion cycle has a volume compression ratio of 14:1.
The pressure and temperature at the beginning of compression are 0.95 bar and $30^{\circ} \mathrm{C}$ respectively. The maximum pressure of the cycle is 44 bar and the constant pressure heat transfer takes place for $1 / 18$ of the stroke.
(a) Sketch the cycle on Pressure-Volume and Temperature-specific entropy diagrams.
(b) Calculate EACH of the following per unit mass of air:
(i) the heat supply;
(ii) the heat rejected;
(iii) the net work output;
(iv) the thermal efficiency.

Note: For air $c_{p}=1.005 \mathrm{~kJ} / \mathrm{kgK} \quad c_{v}=0.718 \mathrm{~kJ} / \mathrm{kgK}$
3. A pure hydrocarbon fuel is completely burned in air.

The dry flue gas analysis shows they contain 15\% carbon dioxide and $2.5 \%$ oxygen by volume.
(a) Determine the full combustion equation in kmols per kmol of fuel.
(b) Calculate EACH of the following:
(i) the percentage mass analysis of the fuel;
(ii) the gravimetric analysis of the wet exhaust gas.

Note: Relative atomic masses $H=1, C=12, N=14, O=16$
Air contains $21 \%$ oxygen by volume.
4. A steam power plant operates between a boiler pressure and temperature of 50 bar and $450^{\circ} \mathrm{C}$ respectively and a condenser pressure of 45 millibar.

The steam expands isentropically from the boiler pressure to a dry saturated condition, at which point some steam is bled off to a direct contact feed heater. The feed water leaves the heater at the saturation temperature of the bled steam pressure.

The remainder of the steam expands isentropically to the condenser pressure. There is 4 K of sub-cooling in the condenser and the feed pump work may be ignored.
(a) Sketch the cycle on a Temperature-specific entropy diagram.
(b) Determine EACH of the following:
(i) the percentage moisture in the turbine exhaust;
(ii) the mass flow rate of bled steam per kg of steam flowing;
(iii) the thermal efficiency of the cycle.
5. The first stage of an impulse turbine is a two row Curtis wheel.

Steam leaves the nozzles at $830 \mathrm{~m} / \mathrm{s}$ and the blade speed is $180 \mathrm{~m} / \mathrm{s}$.
The first row of moving blade rows are symmetrical with a blade angle of $30^{\circ}$. The velocity coefficient of 0.85 for all blade rows.
The outlet angles from the fixed blades and the second row of moving blades are $35^{\circ}$ and $24^{\circ}$ respectively.
(a) Draw to a scale of $1 \mathrm{~mm}=5 \mathrm{~m} / \mathrm{s}$ the velocity diagram for each row.
(b) Determine EACH of the following:
(i) the nozzle angle to the plane of the wheel;
(ii) the inlet angle to the second row of moving blades;
(iii) the power output of the stage per kg of steam flowing;
(iv) the diagram efficiency.
6. The cooling load in a vapour compression refrigeration plant using $\mathrm{CO}_{2}$ is 50 kW . At this load, the refrigerant enters the compressor at a pressure of 17.314 bar and temperature of $-14^{\circ} \mathrm{C}$. It is then compressed isentropically to a pressure of 54.65 bar and temperature of $68^{\circ} \mathrm{C}$.

After cooling the refrigerant enters the expansion valve as a saturated liquid.
The density of the $\mathrm{CO}_{2}$ at the compressor suction is $34.66 \mathrm{~kg} / \mathrm{m}^{3}$.
The four cylinder single acting compressor has a bore and stroke of 100 mm with a volumetric efficiency of $85 \%$.
(a) Sketch the cycle on Pressure-specific enthalpy and Temperature-specific entropy diagrams.
(b) Using Datasheet Q6, calculate EACH of the following:
(i) the mass flow rate of refrigerant;
(ii) the compressor power;
(iii) the coefficient of performance;
(iv) the compressor speed of rotation
7. A furnace wall consists of fire-brick 440 mm thick supported externally by 10 mm thick steel plating.
The internal temperature of the furnace is $1500^{\circ} \mathrm{C}$ and the temperature of the surroundings is $25^{\circ} \mathrm{C}$.
To reduce heat loss it is proposed to remove some of the firebrick and replace it with insulation. However, the maximum temperature the insulation can withstand is $850^{\circ} \mathrm{C}$.

Calculate EACH of the following:
(a) the rate of heat loss per $\mathrm{m}^{2}$ without insulation;
(b) the maximum permissible thickness of the insulation;
(c) the percentage reduction in heat loss when the insulation is fitted.

Note: inner surface heat transfer coefficient $=10 \mathrm{~W} / \mathrm{m}^{2} \mathrm{~K}$ thermal conductivity of the fire-brick $=1.6 \mathrm{~W} / \mathrm{mK}$
thermal conductivity of steel $=50 \mathrm{~W} / \mathrm{mK}$
thermal conductivity of the insulation $=0.45 \mathrm{~W} / \mathrm{mK}$
outer surface heat transfer coefficient $=5 \mathrm{~W} / \mathrm{m}^{2} \mathrm{~K}$
8. A two-stage, single acting reciprocating compressor has a clearance volume of $4.5 \%$ of the swept volume in each stage. It is used to compress methane $\left(\mathrm{CH}_{4}\right)$. The initial pressure and temperature are 0.95 bar and $25^{\circ} \mathrm{C}$ respectively and the maximum temperature of the methane must be limited to $150^{\circ} \mathrm{C}$.
The polytropic index for each compression and expansion process process is 1.3 and inter-cooling is perfect.
(a) Sketch the process on a Pressure-Volume diagram indicating the work saved by inter-cooling.
(b) Calculate EACH of the following:
(i) the interstage and delivery pressures;
(ii) the volumetric efficiency of each stage;
(iii) the specific work input;
(iv) the isothemal efficiency.

Note: Relative atomic masses $\mathrm{H}=1, \mathrm{C}=12$
The universal gas constant $=8.3145 \mathrm{~kJ} / \mathrm{kmolK}$
9. The volume of the shell of a steam condenser is $14.5 \mathrm{~m}^{3}$. The shell contains saturated water, dry saturated steam and air, all at a temperature of $39^{\circ} \mathrm{C}$ and vacuum gauge reading of 672 mm of mercury. The mass of water present is 112 grammes.
After a period of time the temperature of the condenser shell rises to $50^{\circ} \mathrm{C}$.
The atmospheric pressure remains constant at 996 mbar throughout the temperature change.

Determine EACH of the following:
(a) the mass of air present;
(b) the mass of dry saturated vapour;
(c) the partial pressure of the steam at $50^{\circ} \mathrm{C}$;
(d) the condition of the steam at $50^{\circ} \mathrm{C}$;
(e) the condenser pressure at $50^{\circ} \mathrm{C}$.

Note : for air $\mathrm{R}=0.287 \mathrm{~kJ} / \mathrm{kgK}$ 1 bar $=750 \mathrm{~mm} \mathrm{Hg}$
refrigerant: $\mathrm{CO}_{2}$

| saturation values |  |  |  |  |  |  | superheat ( $T-T_{s}$ ) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  | 50 K |  | 100 K |  |
| $\begin{gathered} \mathrm{T} \\ \left({ }^{\circ} \mathrm{C}\right) \end{gathered}$ | $\begin{gathered} \mathbf{p}_{\mathbf{s}} \\ \text { (bar) } \\ \hline \end{gathered}$ | $\begin{gathered} \mathbf{v}_{\mathbf{g}} \\ \left(\mathrm{m}^{3} / \mathrm{kg}\right) \end{gathered}$ | $\overline{\mathbf{h}_{f}}$ <br> (k |  |  |  | $\begin{gathered} \hline \mathbf{h} \\ (\mathrm{kJ} / \mathrm{kg}) \\ \hline \end{gathered}$ | $\begin{gathered} \mathbf{s} \\ (\mathrm{kJ} /(\mathrm{kg} \mathrm{~K})) \end{gathered}$ | $\begin{gathered} \mathbf{h} \\ (\mathrm{kJ} / \mathrm{kg}) \end{gathered}$ | $\begin{gathered} \hline \mathbf{s} \\ (\mathrm{kJ} /(\mathrm{kg} \mathrm{~K})) \end{gathered}$ |
| -50 | 6.8234 | 0.0558 | -19.96 | 319.77 | -0.0863 | 1.4362 | 365.1 | 1.620 | 409.9 | 1.770 |
| -45 | 8.3184 | 0.0460 | -10.03 | 321.23 | -0.0428 | 1.4091 | 367.81 | 1.594 | 413.26 | 1.744 |
| -40 | 10.0450 | 0.0383 | 0.00 | 322.42 | 0.0000 | 1.3829 | 370.35 | 1.569 | 416.53 | 1.720 |
| -35 | 12.0242 | 0.0320 | 10.15 | 323.33 | 0.0423 | 1.3574 | 372.75 | 1.546 | 419.70 | 1.696 |
| -30 | 14.2776 | 0.0270 | 20.43 | 323.92 | 0.0842 | 1.3323 | 375.00 | 1.524 | 422.77 | 1.674 |
| -28 | 15.2607 | 0.0252 | 24.60 | 324.06 | 0.1009 | 1.3224 | 375.85 | 1.515 | 423.97 | 1.666 |
| -26 | 16.2926 | 0.0236 | 28.78 | 324.14 | 0.1175 | 1.3125 | 376.68 | 1.507 | 425.15 | 1.657 |
| -24 | 17.3749 | 0.0220 | 33.00 | 324.15 | 0.1341 | 1.3026 | 377.48 | 1.498 | 426.31 | 1.649 |
| -22 | 18.5089 | 0.0206 | 37.26 | 324.11 | 0.1506 | 1.2928 | 378.25 | 1.490 | 427.45 | 1.641 |
| -20 | 19.6963 | 0.0193 | 41.55 | 323.99 | 0.1672 | 1.2829 | 378.99 | 1.482 | 428.58 | 1.633 |
| -18 | 20.9384 | 0.0181 | 45.87 | 323.80 | 0.1837 | 1.2730 | 379.70 | 1.474 | 429.68 | 1.626 |
| -16 | 22.2370 | 0.0170 | 50.24 | 323.53 | 0.2003 | 1.2631 | 380.39 | 1.466 | 430.77 | 1.618 |
| -14 | 23.5935 | 0.0159 | 54.65 | 323.19 | 0.2169 | 1.2531 | 381.04 | 1.458 | 431.83 | 1.610 |
| -12 | 25.0095 | 0.0150 | 59.11 | 322.76 | 0.2334 | 1.2430 | 381.66 | 1.450 | 432.88 | 1.603 |
| -10 | 26.4868 | 0.0140 | 63.62 | 322.23 | 0.2501 | 1.2328 | 382.25 | 1.443 | 433.90 | 1.596 |
| -8 | 28.0269 | 0.0132 | 68.18 | 321.61 | 0.2668 | 1.2226 | 382.81 | 1.435 | 434.91 | 1.589 |
| -6 | 29.6316 | 0.0124 | 72.81 | 320.89 | 0.2835 | 1.2121 | 383.34 | 1.428 | 435.89 | 1.582 |
| -4 | 31.3027 | 0.0116 | 77.50 | 320.05 | 0.3003 | 1.2015 | 383.83 | 1.420 | 436.85 | 1.575 |
| -2 | 33.0420 | 0.0109 | 82.26 | 319.09 | 0.3173 | 1.1907 | 384.29 | 1.413 | 437.79 | 1.568 |
| 0 | 34.8514 | 0.0102 | 87.10 | 317.99 | 0.3344 | 1.1797 | 384.71 | 1.405 | 438.71 | 1.561 |
| 2 | 36.7329 | 0.0096 | 92.02 | 316.75 | 0.3516 | 1.1683 | 385.10 | 1.398 | 439.61 | 1.554 |
| 4 | 38.6884 | 0.0090 | 97.05 | 315.35 | 0.3690 | 1.1567 | 385.45 | 1.391 | 440.49 | 1.548 |
| 6 | 40.7202 | 0.0084 | 102.18 | 313.77 | 0.3866 | 1.1446 | 385.77 | 1.384 | 441.34 | 1.541 |
| 8 | 42.8306 | 0.0079 | 107.43 | 311.99 | 0.4045 | 1.1321 | 386.05 | 1.377 | 442.17 | 1.535 |
| 10 | 45.0218 | 0.0074 | 112.83 | 309.98 | 0.4228 | 1.1190 | 386.29 | 1.369 | 442.97 | 1.528 |
| 12 | 47.2966 | 0.0069 | 118.38 | 307.72 | 0.4414 | 1.1053 | 386.49 | 1.362 | 443.76 | 1.522 |
| 14 | 49.6577 | 0.0064 | 124.13 | 305.15 | 0.4605 | 1.0909 | 386.65 | 1.355 | 444.51 | 1.516 |
| 16 | 52.1080 | 0.0060 | 130.11 | 302.22 | 0.4802 | 1.0754 | 386.77 | 1.348 | 445.25 | 1.509 |
| 18 | 54.6511 | 0.0056 | 136.36 | 298.86 | 0.5006 | 1.0588 | 386.85 | 1.341 | 445.95 | 1.503 |
| 20 | 57.2905 | 0.0051 | 142.97 | 294.96 | 0.5221 | 1.0406 | 386.88 | 1.334 | 446.64 | 1.497 |
| 22 | 60.0308 | 0.0047 | 150.02 | 290.36 | 0.5449 | 1.0203 | 386.87 | 1.327 | 447.29 | 1.491 |
| 24 | 62.8773 | 0.0043 | 157.71 | 284.80 | 0.5695 | 0.9972 | 386.81 | 1.320 | 447.91 | 1.485 |
| 26 | 65.8368 | 0.0039 | 166.36 | 277.80 | 0.5971 | 0.9697 | 386.70 | 1.313 | 448.51 | 1.478 |
| 28 | 68.9182 | 0.0035 | 176.72 | 268.30 | 0.6301 | 0.9342 | 386.53 | 1.305 | 449.07 | 1.472 |
| 30 | 72.1369 | 0.0029 | 191.65 | 252.23 | 0.6778 | 0.8776 | 386.30 | 1.298 | 449.58 | 1.466 |
| 30.98 | 73.7730 | 0.0021 | 219.34 | 219.34 | 0.7680 | 0.7680 | 386.15 | 1.294 | 449.82 | 1.463 |

