# CERTIFICATES OF COMPETENCY IN THE MERCHANT NAVY MARINE ENGINEER OFFICER 

EXAMINATIONS ADMINISTERED BY THE
SCOTTISH QUALIFICATIONS AUTHORITY
ON BEHALF OF THE
MARITIME AND COASTGUARD AGENCY

## STCW 95 CHIEF ENGINEER REG. III/2 (UNLIMITED)

## 041-32 - APPLIED HEAT

MONDAY 12 DECEMBER 2011
1315-1615 hrs

Examination paper inserts:
Datasheet Q6 (Property table for $\mathrm{CO}_{2}$ )

Notes for the guidance of candidates:

1. Non-programmable calculators may be used.
2. All formulae used must be stated and the method of working and ALL intermediate steps must be made clear in the answer.

Materials to be supplied by examination centres:
Candidates examination workbook
Graph paper
'Thermodynamic and Transport Properties of Fluids' by Mayhew \& Rogers (5 ${ }^{\text {th }}$ edition)

## APPLIED HEAT

## Attempt SIX questions only.

## All questions carry equal marks.

Marks for each part question are shown in brackets.

1. Ideal gas in a cylinder is cooled at constant pressure from a temperature of $1200^{\circ} \mathrm{C}$ to a temperature of $800^{\circ} \mathrm{C}$, and then further cooled at constant volume from $800^{\circ} \mathrm{C}$ to $500^{\circ} \mathrm{C}$. The change in specific entropy in the second process is $-3.326 \mathrm{~kJ} / \mathrm{kg} \mathrm{K}$. After being cooled, the gas is compressed isentropically to the initial pressure and a temperature of $577.3^{\circ} \mathrm{C}$.
(a) Sketch the processes on $\mathrm{p}-\mathrm{V}$ and T-s diagrams.
(b) Determine EACH of the following:
(i) the values of $\mathrm{c}_{\mathrm{V}}, \mathrm{c}_{\mathrm{P}}, \mathrm{R}$ and $\gamma$ for the gas;
(ii) the change in specific entropy during the constant pressure process;
(iii) the work transfer per kg of gas during isentropic compression.
2. In an air standard dual combustion cycle, the volume compression ratio is $26 / 1$. The maximum and minimum temperatures are 2200 K and 305 K respectively. The maximum and minimum pressures are respectively 110 bar and 1.02 bar .
(a) Sketch the cycle on $\mathrm{p}-\mathrm{V}$ and T-S diagrams.
(b) Determine EACH of the following:
(i) the thermal efficiency;
(ii) the mean effective pressure.

Note: $\quad$ For air, $\gamma=1.4$ and $c_{P}=1.005 \mathrm{~kJ} / \mathrm{kg} \mathrm{K}$.
3. The volumetric analysis of a gaseous fuel is: methane $\left(\mathrm{CH}_{4}\right) 50 \%$; ethane $\left(\mathrm{C}_{2} \mathrm{H}_{6}\right) 30 \%$; ethylene $\left(\mathrm{C}_{2} \mathrm{H}_{4}\right) 20 \%$. The dry combustion products contain $3 \% \mathrm{CO}$ and $6 \% \mathrm{O}_{2}$ by volume.
(a) Formulate the full combustion equation per kmol of fuel.
(b) Determine the percentage excess air supplied.

Note: atomic mass relationships: $H=1 ; C=12 ; O=16 ; N=14$ Air contains $21 \%$ oxygen by volume.
4. (a) A Carnot cycle uses saturated water and steam as the working fluid, and operates between pressures of 0.045 bar and 44 bar . At the beginning of heat supply, the state of the fluid is saturated liquid, and at the end of heat supply it is dry saturated vapour.
(i) Sketch the cycle on $\mathrm{p}-\mathrm{V}$ and T -s diagrams.
(ii) Determine the thermal efficiency of the cycle.
(iii) Determine the specific work output of the cycle.
(b) An ideal Rankine cycle using steam operates between the same pressures as the Carnot cycle in Q4(a). The steam is dry saturated at the beginning of expansion, and saturated liquid leaves the condenser.
(i) Sketch the cycle on the T-s diagram.
(ii) Determine the specific work output of the cycle, allowing for feed pump work.
(iii) Determine the thermal efficiency of the cycle.
5. The drop in specific enthalpy as steam passes through the nozzles of a two-row velocity compounded impulse turbine stage is $500 \mathrm{~kJ} / \mathrm{kg}$. The nozzle angle is $18^{\circ}$ and the mean blade velocity is $225 \mathrm{~m} / \mathrm{s}$. All the blades are symmetrical, and the blade friction coefficient is 0.9 for all blades.
(a) Sketch the velocity diagrams for each moving row, labelling all velocities and angles.
(b) Determine EACH of the following:
(i) all the blade angles;
(ii) the blade work per kg .
6. A vapour compression cooling cycle using $\mathrm{CO}_{2}$ operates between pressures of 20.9384 bar and 72.1369 bar. The refrigerant enters the compressor at a temperature of $-13^{\circ} \mathrm{C}$ and leaves the condenser as a saturated liquid. The isentropic efficiency of the compressor is 85\%.
(a) Sketch the cycle on p-h and T-s diagrams.
(b) Using Datasheet Q6, determine the coefficient of performance of the cycle.
(c) State TWO disadvantages and TWO advantages of $\mathrm{CO}_{2}$ compared with other refrigerants.
7. An LNG carrier has three spherical tanks each of diameter 44 m . They contain liquefied gas at a temperature of $-163^{\circ} \mathrm{C}$. The tanks are insulated with a 300 mm thickness of material of thermal conductivity $0.04 \mathrm{~W} / \mathrm{m} \mathrm{K}$. The outside surface heat transfer coefficient is $12 \mathrm{~W} / \mathrm{m}^{2} \mathrm{~K}$, and the temperature of the surrounding air is $30^{\circ} \mathrm{C}$. The thermal resistances of the inside surface film and of the tank wall may be disregarded. The latent heat of evaporation of the gas is $510 \mathrm{~kJ} / \mathrm{kg}$.

Determine the mass of gas which boils off each day.
8. At the beginning of compression in a single stage, single acting reciprocating air compressor, the air is at a pressure of 0.99 bar and a temperature of $15^{\circ} \mathrm{C}$. The delivery valve opens at a pressure of 5.8 bar. The delivery temperature is $151^{\circ} \mathrm{C}$. The bore diameter and stroke length are 0.28 m and 0.30 m respectively. The clearance volume is $5 \%$ of the swept volume and the compressor runs at $400 \mathrm{rev} / \mathrm{min}$.
(a) Sketch the $\mathrm{p}-\mathrm{V}$ diagram.
(b) Determine EACH of the following:
(i) the index of compression;
(ii) the volumetric efficiency;
(iii) the indicated work per kg of air;
(iv) the free air capacity in $\mathrm{m}^{3} / \mathrm{min}$, given that free air conditions are 1.013 bar and $25^{\circ} \mathrm{C}$.

Note: $\quad$ For air, $R=0.287 \mathrm{~kJ} / \mathrm{kg}$ K.
9. (a) Explain why impulse turbine nozzles have convergent-divergent form.
(b) Air expands isentropically in a convergent-divergent nozzle. The pressure at nozzle inlet is 15 bar and the inlet temperature is 450 K . The outlet pressure is 5 bar. The mass flow rate is $6.5 \mathrm{~kg} / \mathrm{s}$.

Determine EACH of the following:
(i) the throat area;
(ii) the exit area.

Note: $\quad p_{c}=p_{0} \times\left(\frac{2}{\gamma+1}\right)^{\gamma /(\gamma-1)} ; \quad T_{c}=T_{0} \times\left(\frac{2}{\gamma+1}\right) ; \quad a=\sqrt{\gamma R T}$
For air, $R=0.287 \mathrm{~kJ} / \mathrm{kg} \mathrm{K}$ and $\gamma=1.4$.
refrigerant: $\mathrm{CO}_{2}$

| saturation values |  |  |  |  |  |  | superheat ( $T-T_{s}$ ) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  | 50 K |  | 100 K |  |
| $\begin{gathered} \hline \mathbf{T} \\ \left({ }^{\circ} \mathrm{C}\right) \\ \hline \end{gathered}$ | $\begin{gathered} \hline \mathbf{p}_{\mathbf{s}} \\ \text { (bar) } \end{gathered}$ | $\begin{gathered} \mathbf{v}_{\mathbf{g}} \\ \left(\mathrm{m}^{3} / \mathrm{kg}\right) \end{gathered}$ | $(\mathrm{kJ} / \mathrm{kg})^{\text {a }}$ |  | (kJ/(kg K)) |  | $\begin{gathered} \hline \mathbf{h} \\ (\mathrm{kJ} / \mathrm{kg}) \\ \hline \end{gathered}$ | $\begin{gathered} \mathbf{s} \\ (\mathrm{kJ} /(\mathrm{kg} \mathrm{~K})) \end{gathered}$ | $\begin{gathered} \hline \mathbf{h} \\ (\mathrm{kJ} / \mathrm{kg}) \\ \hline \end{gathered}$ | $\begin{gathered} \mathbf{s} \\ (\mathrm{kJ} /(\mathrm{kg} \mathrm{~K})) \end{gathered}$ |
| -50 | 6.8234 | 0.0558 | -19.96 | 319.77 | -0.0863 | 1.4362 | 365.1 | 1.620 | 409.9 | 1.770 |
| -45 | 8.3184 | 0.0460 | -10.03 | 321.23 | -0.0428 | 1.4091 | 367.81 | 1.594 | 413.26 | 1.744 |
| -40 | 10.0450 | 0.0383 | 0.00 | 322.42 | 0.0000 | 1.3829 | 370.35 | 1.569 | 416.53 | 1.720 |
| -35 | 12.0242 | 0.0320 | 10.15 | 323.33 | 0.0423 | 1.3574 | 372.75 | 1.546 | 419.70 | 1.696 |
| -30 | 14.2776 | 0.0270 | 20.43 | 323.92 | 0.0842 | 1.3323 | 375.00 | 1.524 | 422.77 | 1.674 |
| -28 | 15.2607 | 0.0252 | 24.60 | 324.06 | 0.1009 | 1.3224 | 375.85 | 1.515 | 423.97 | 1.666 |
| -26 | 16.2926 | 0.0236 | 28.78 | 324.14 | 0.1175 | 1.3125 | 376.68 | 1.507 | 425.15 | 1.657 |
| -24 | 17.3749 | 0.0220 | 33.00 | 324.15 | 0.1341 | 1.3026 | 377.48 | 1.498 | 426.31 | 1.649 |
| -22 | 18.5089 | 0.0206 | 37.26 | 324.11 | 0.1506 | 1.2928 | 378.25 | 1.490 | 427.45 | 1.641 |
| -20 | 19.6963 | 0.0193 | 41.55 | 323.99 | 0.1672 | 1.2829 | 378.99 | 1.482 | 428.58 | 1.633 |
| -18 | 20.9384 | 0.0181 | 45.87 | 323.80 | 0.1837 | 1.2730 | 379.70 | 1.474 | 429.68 | 1.626 |
| -16 | 22.2370 | 0.0170 | 50.24 | 323.53 | 0.2003 | 1.2631 | 380.39 | 1.466 | 430.77 | 1.618 |
| -14 | 23.5935 | 0.0159 | 54.65 | 323.19 | 0.2169 | 1.2531 | 381.04 | 1.458 | 431.83 | 1.610 |
| -12 | 25.0095 | 0.0150 | 59.11 | 322.76 | 0.2334 | 1.2430 | 381.66 | 1.450 | 432.88 | 1.603 |
| -10 | 26.4868 | 0.0140 | 63.62 | 322.23 | 0.2501 | 1.2328 | 382.25 | 1.443 | 433.90 | 1.596 |
| -8 | 28.0269 | 0.0132 | 68.18 | 321.61 | 0.2668 | 1.2226 | 382.81 | 1.435 | 434.91 | 1.589 |
| -6 | 29.6316 | 0.0124 | 72.81 | 320.89 | 0.2835 | 1.2121 | 383.34 | 1.428 | 435.89 | 1.582 |
| -4 | 31.3027 | 0.0116 | 77.50 | 320.05 | 0.3003 | 1.2015 | 383.83 | 1.420 | 436.85 | 1.575 |
| -2 | 33.0420 | 0.0109 | 82.26 | 319.09 | 0.3173 | 1.1907 | 384.29 | 1.413 | 437.79 | 1.568 |
| 0 | 34.8514 | 0.0102 | 87.10 | 317.99 | 0.3344 | 1.1797 | 384.71 | 1.405 | 438.71 | 1.561 |
| 2 | 36.7329 | 0.0096 | 92.02 | 316.75 | 0.3516 | 1.1683 | 385.10 | 1.398 | 439.61 | 1.554 |
| 4 | 38.6884 | 0.0090 | 97.05 | 315.35 | 0.3690 | 1.1567 | 385.45 | 1.391 | 440.49 | 1.548 |
| 6 | 40.7202 | 0.0084 | 102.18 | 313.77 | 0.3866 | 1.1446 | 385.77 | 1.384 | 441.34 | 1.541 |
| 8 | 42.8306 | 0.0079 | 107.43 | 311.99 | 0.4045 | 1.1321 | 386.05 | 1.377 | 442.17 | 1.535 |
| 10 | 45.0218 | 0.0074 | 112.83 | 309.98 | 0.4228 | 1.1190 | 386.29 | 1.369 | 442.97 | 1.528 |
| 12 | 47.2966 | 0.0069 | 118.38 | 307.72 | 0.4414 | 1.1053 | 386.49 | 1.362 | 443.76 | 1.522 |
| 14 | 49.6577 | 0.0064 | 124.13 | 305.15 | 0.4605 | 1.0909 | 386.65 | 1.355 | 444.51 | 1.516 |
| 16 | 52.1080 | 0.0060 | 130.11 | 302.22 | 0.4802 | 1.0754 | 386.77 | 1.348 | 445.25 | 1.509 |
| 18 | 54.6511 | 0.0056 | 136.36 | 298.86 | 0.5006 | 1.0588 | 386.85 | 1.341 | 445.95 | 1.503 |
| 20 | 57.2905 | 0.0051 | 142.97 | 294.96 | 0.5221 | 1.0406 | 386.88 | 1.334 | 446.64 | 1.497 |
| 22 | 60.0308 | 0.0047 | 150.02 | 290.36 | 0.5449 | 1.0203 | 386.87 | 1.327 | 447.29 | 1.491 |
| 24 | 62.8773 | 0.0043 | 157.71 | 284.80 | 0.5695 | 0.9972 | 386.81 | 1.320 | 447.91 | 1.485 |
| 26 | 65.8368 | 0.0039 | 166.36 | 277.80 | 0.5971 | 0.9697 | 386.70 | 1.313 | 448.51 | 1.478 |
| 28 | 68.9182 | 0.0035 | 176.72 | 268.30 | 0.6301 | 0.9342 | 386.53 | 1.305 | 449.07 | 1.472 |
| 30 | 72.1369 | 0.0029 | 191.65 | 252.23 | 0.6778 | 0.8776 | 386.30 | 1.298 | 449.58 | 1.466 |
| 30.98 | 73.7730 | 0.0021 | 219.34 | 219.34 | 0.7680 | 0.7680 | 386.15 | 1.294 | 449.82 | 1.463 |

based on data from NIST: www.nist.gov

