# CERTIFICATES OF COMPETENCY IN THE MERCHANT NAVY MARINE ENGINEER OFFICER 

EXAMINATIONS ADMINISTERED BY THE<br>SCOTTISH QUALIFICATIONS AUTHORITY<br>ON BEHALF OF THE<br>MARITIME AND COASTGUARD AGENCY<br>\section*{STCW 95 CHIEF ENGINEER REG. III/2 (UNLIMITED)}

041-32 - APPLIED HEAT

MONDAY, 18 OCTOBER 2010
1315-1615 hrs

Examination paper inserts:
Datasheet Q6 - Property table for $\mathrm{CO}_{2}$

Notes for the guidance of candidates:

1. Non-programmable calculators may be used.
2. All formulae used must be stated and the method of working and ALL intermediate steps must be made clear in the answer.

Materials to be supplied by examination centres:
Candidates' examination workbook
Graph paper
'Thermodynamic and Transport Properties of Fluids' by Mayhew \& Rogers ( $5{ }^{\text {th }}$ edition)

## APPLIED HEAT

## Attempt SIX questions only.

## All questions carry equal marks.

## Marks for each part question are shown in brackets.

1. A perfect gas for which $\mathrm{R}=0.287 \mathrm{~kJ} / \mathrm{kg} \mathrm{K}$ and $\gamma=1.33$ expands reversibly in a cylinder according to the law $\mathrm{pV}^{1.48}=$ constant and then heated at constant volume. The initial pressure is 88 bar, the initial temperature is $1727^{\circ} \mathrm{C}$ and the final pressure is 1.5 bar . The final volume is twenty times the initial volume.
(a) Sketch the processes on p-V and T-S diagrams.
(b) Determine EACH of the following:
(i) the temperature after expansion;
(ii) the final temperature;
(ii) the net heat transfer per kg ;
(iv) the net change in specific entropy.
2. The following data refer to a 20 cylinder 4 -stroke diesel engine under test:

| bore diameter | 280 mm |
| :--- | :--- |
| stroke length | 330 mm |
| speed of rotation | $1000 \mathrm{rev} / \mathrm{min}$ |
| brake torque | 86 kN m |
| fuel consumption | 1.71 tonne $/ \mathrm{h}$ |
| calorific value of fuel | $42 \mathrm{MJ} / \mathrm{kg}$ |

The fuel supply to each cylinder is cut off in turn, and the brake torque is adjusted each time so that the speed returns to $1000 \mathrm{rev} / \mathrm{min}$. The mean value of the torques thus measured is 81.23 kN m .

Determine EACH of the following:
(a) the brake power;
(b) the mechanical efficiency;
(c) the brake specific fuel consumption $(\mathrm{kg} / \mathrm{kW} \mathrm{h})$;
(d) the average value of indicated mean effective pressure;
(e) the brake thermal efficiency.
3. The mass analysis of a fuel is: carbon $78 \%$; hydrogen $16 \%$; sulphur $3.2 \%$; water $2 \%$ (remainder ash).

Determine EACH of the following:
(a) the theoretical air/fuel ratio by mass;
(b) the volumetric analysis of the dry products (ie excluding $\mathrm{H}_{2} \mathrm{O}$ and soluble $\mathrm{SO}_{2}$ ) when the fuel is burned completely in $30 \%$ excess air;
(c) the dew point temperature of the combustion products if the total pressure is 1.03 bar.

Note: atomic mass relationships: $H=1 ; C=12 ; O=16 ; N=14 ; S=32$ Air contains $21 \%$ oxygen by volume and $23.3 \%$ oxygen by mass.
4. A steam power plant consists of turbine, condenser, feed pump and boiler. Steam enters the turbine at a pressure of 50 bar and a temperature of $400^{\circ} \mathrm{C}$, and expands to 0.2 bar, dryness fraction 0.9 . The steam is then fully condensed without undercooling. Feed pump work may be disregarded. The boiler has an efficiency of $87 \%$. The fuel used has a calorific value of $38 \mathrm{MJ} / \mathrm{kg}$ and contains $85 \%$ carbon by mass.

It is proposed that the plant be modified to incorporate "carbon capture", which involves separating the $\mathrm{CO}_{2}$ from the exhaust gas and pumping it to a storage facility. It is estimated that separating the $\mathrm{CO}_{2}$ from the flue gases will require $19 \%$ of the turbine power output, and pumping the $\mathrm{CO}_{2}$ will require 40 kJ per kg of $\mathrm{CO}_{2}$.

Determine the overall thermal efficiency of the plant:
(a) before modification;
(b) after modification.

Note: relative atomic masses: $C=12 ; O=16$
5. (a) Define the term degree of reaction relating to a turbine stage.
(b) In a $50 \%$ reaction turbine stage the steam leaves the fixed blades with a velocity of $280 \mathrm{~m} / \mathrm{s}$. The axial velocity component is $148.3 \mathrm{~m} / \mathrm{s}$ and the blade velocity is $200 \mathrm{~m} / \mathrm{s}$.

Determine EACH of the following:
(i) the blade inlet and outlet angles;
(ii) the blade work per kg;
(iii) the diagram efficiency.
6. A vapour compression cooling cycle using $\mathrm{CO}_{2}$ operates between pressures of 18.5089 bar and 68.9182 bar. The refrigerant enters the compressor at a temperature of $-18^{\circ} \mathrm{C}$ and leaves the condenser as saturated liquid. The temperature at compressor outlet is $103^{\circ} \mathrm{C}$.
(a) Sketch the cycle on a p-h diagram.
(b) Using Datasheet Q6, determine the coefficient of performance of the cycle.
(c) State TWO disadvantages and THREE advantages of $\mathrm{CO}_{2}$ as a refrigerant compared with other refrigerants such as halocarbons, hydrocarbons and ammonia.
7. Wet steam at a pressure of 7.0 bar flows in a 5 m long pipe of inside diameter 38 mm and wall thickness 5 mm . The pipe is surrounded with a layer of lagging 15 mm thick. The thermal conductivity of the lagging is $0.05 \mathrm{~W} / \mathrm{m} \mathrm{K}$ and the outside surface heat transfer coefficient is $12 \mathrm{~W} / \mathrm{m}^{2} \mathrm{~K}$. The outside air temperature is $30^{\circ} \mathrm{C}$. The thermal resistances of steam film and pipe wall may be disregarded.

Determine EACH of the following:
(a) the rate of heat loss;
(b) the outside surface temperature of the lagging;
(c) the increase in the rate of heat loss which would result if the thickness of the lagging were reduced to 10 mm .
8. A reciprocating compressor is to be used to compress methane $\left(\mathrm{CH}_{4}\right)$ which enters at a temperature of 300 K and a pressure of 0.95 bar. For safety reasons, the temperature of the methane is not to exceed 400 K . The index of compression is 1.3.

Determine EACH of the following:
(a) the specific gas constant $R$ for methane;
(b) the maximum pressure which can safely be obtained in a single stage;
(c) the volumetric efficiency of the single stage machine if the clearance volume is $4.5 \%$ of the swept volume:
(d) the maximum pressure which can safely be obtained using two stages with perfect intercooling;
(e) the isothermal efficiency of the two stage machine.

Note: atomic mass relationships: $H=1 ; C=12$
The universal gas constant is $8.314 \mathrm{~kJ} / \mathrm{kmol} \mathrm{K}$
9. (a) Explain the term choked flow with reference to a convergent nozzle.
(b) Air leaks into an evacuated vessel from the surroundings which are at a pressure of 1.00 bar. The passage through which the air leaks may be considered as a convergent nozzle with exit area $0.8 \mathrm{~mm}^{2}$, and the flow within the passage may be assumed isentropic. The temperature of the surroundings is $25^{\circ} \mathrm{C}$.

Determine the mass flow rate when the pressure in the vessel is:
(i) 0.5 bar ;
(ii) 0.8 bar .

Note: $\quad$ For air, $\gamma=1.4$ and $R=0.287 \mathrm{~kJ} / \mathrm{kg} K$

$$
p_{c}=p_{0} \times\left(\frac{2}{\gamma+1}\right)^{\gamma /(\gamma-1)} ; \quad a=\sqrt{\gamma R T}
$$

refrigerant: $\mathrm{CO}_{2}$

| saturation values |  |  |  |  |  |  | superheat ( $T-T_{s}$ ) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  | 50 K |  | 100 K |  |
| $\begin{gathered} \mathbf{T} \\ \left({ }^{\circ} \mathrm{C}\right) \\ \hline \end{gathered}$ | $\begin{gathered} \mathbf{p}_{\mathbf{s}} \\ (\mathrm{bar}) \end{gathered}$ | $\begin{gathered} \mathbf{v}_{\mathbf{g}} \\ \left(\mathrm{m}^{3} / \mathrm{kg}\right) \\ \hline \end{gathered}$ | $\begin{array}{ll} \hline \mathbf{h}_{\mathbf{f}} \quad \\ \quad(\mathrm{k}) \\ \hline \end{array}$ |  | $\mathbf{s}_{\mathbf{f}}$ $(\mathrm{kJ} /($ | (kJ/(kg K)) | $\begin{gathered} \mathbf{h} \\ (\mathrm{kJ} / \mathrm{kg}) \end{gathered}$ | $\begin{gathered} \hline \mathbf{s} \\ (\mathrm{kJ} /(\mathrm{kg} \mathrm{~K})) \end{gathered}$ | $\begin{gathered} \hline \mathbf{h} \\ (\mathrm{kJ} / \mathrm{kg}) \\ \hline \end{gathered}$ | $\begin{gathered} \hline \mathbf{s} \\ (\mathrm{kJ} /(\mathrm{kg} \mathrm{~K})) \end{gathered}$ |
| -50 | 6.8234 | 0.0558 | -19.96 | 319.77 | -0.0863 | 1.4362 | 365.1 | 1.620 | 409.9 | 1.770 |
| -45 | 8.3184 | 0.0460 | -10.03 | 321.23 | -0.0428 | 1.4091 | 367.81 | 1.594 | 413.26 | 1.744 |
| -40 | 10.0450 | 0.0383 | 0.00 | 322.42 | 0.0000 | 1.3829 | 370.35 | 1.569 | 416.53 | 1.720 |
| -35 | 12.0242 | 0.0320 | 10.15 | 323.33 | 0.0423 | 1.3574 | 372.75 | 1.546 | 419.70 | 1.696 |
| -30 | 14.2776 | 0.0270 | 20.43 | 323.92 | 0.0842 | 1.3323 | 375.00 | 1.524 | 422.77 | 1.674 |
| -28 | 15.2607 | 0.0252 | 24.60 | 324.06 | 0.1009 | 1.3224 | 375.85 | 1.515 | 423.97 | 1.666 |
| -26 | 16.2926 | 0.0236 | 28.78 | 324.14 | 0.1175 | 1.3125 | 376.68 | 1.507 | 425.15 | 1.657 |
| -24 | 17.3749 | 0.0220 | 33.00 | 324.15 | 0.1341 | 1.3026 | 377.48 | 1.498 | 426.31 | 1.649 |
| -22 | 18.5089 | 0.0206 | 37.26 | 324.11 | 0.1506 | 1.2928 | 378.25 | 1.490 | 427.45 | 1.641 |
| -20 | 19.6963 | 0.0193 | 41.55 | 323.99 | 0.1672 | 1.2829 | 378.99 | 1.482 | 428.58 | 1.633 |
| -18 | 20.9384 | 0.0181 | 45.87 | 323.80 | 0.1837 | 1.2730 | 379.70 | 1.474 | 429.68 | 1.626 |
| -16 | 22.2370 | 0.0170 | 50.24 | 323.53 | 0.2003 | 1.2631 | 380.39 | 1.466 | 430.77 | 1.618 |
| -14 | 23.5935 | 0.0159 | 54.65 | 323.19 | 0.2169 | 1.2531 | 381.04 | 1.458 | 431.83 | 1.610 |
| -12 | 25.0095 | 0.0150 | 59.11 | 322.76 | 0.2334 | 1.2430 | 381.66 | 1.450 | 432.88 | 1.603 |
| -10 | 26.4868 | 0.0140 | 63.62 | 322.23 | 0.2501 | 1.2328 | 382.25 | 1.443 | 433.90 | 1.596 |
| -8 | 28.0269 | 0.0132 | 68.18 | 321.61 | 0.2668 | 1.2226 | 382.81 | 1.435 | 434.91 | 1.589 |
| -6 | 29.6316 | 0.0124 | 72.81 | 320.89 | 0.2835 | 1.2121 | 383.34 | 1.428 | 435.89 | 1.582 |
| -4 | 31.3027 | 0.0116 | 77.50 | 320.05 | 0.3003 | 1.2015 | 383.83 | 1.420 | 436.85 | 1.575 |
| -2 | 33.0420 | 0.0109 | 82.26 | 319.09 | 0.3173 | 1.1907 | 384.29 | 1.413 | 437.79 | 1.568 |
| 0 | 34.8514 | 0.0102 | 87.10 | 317.99 | 0.3344 | 1.1797 | 384.71 | 1.405 | 438.71 | 1.561 |
| 2 | 36.7329 | 0.0096 | 92.02 | 316.75 | 0.3516 | 1.1683 | 385.10 | 1.398 | 439.61 | 1.554 |
| 4 | 38.6884 | 0.0090 | 97.05 | 315.35 | 0.3690 | 1.1567 | 385.45 | 1.391 | 440.49 | 1.548 |
| 6 | 40.7202 | 0.0084 | 102.18 | 313.77 | 0.3866 | 1.1446 | 385.77 | 1.384 | 441.34 | 1.541 |
| 8 | 42.8306 | 0.0079 | 107.43 | 311.99 | 0.4045 | 1.1321 | 386.05 | 1.377 | 442.17 | 1.535 |
| 10 | 45.0218 | 0.0074 | 112.83 | 309.98 | 0.4228 | 1.1190 | 386.29 | 1.369 | 442.97 | 1.528 |
| 12 | 47.2966 | 0.0069 | 118.38 | 307.72 | 0.4414 | 1.1053 | 386.49 | 1.362 | 443.76 | 1.522 |
| 14 | 49.6577 | 0.0064 | 124.13 | 305.15 | 0.4605 | 1.0909 | 386.65 | 1.355 | 444.51 | 1.516 |
| 16 | 52.1080 | 0.0060 | 130.11 | 302.22 | 0.4802 | 1.0754 | 386.77 | 1.348 | 445.25 | 1.509 |
| 18 | 54.6511 | 0.0056 | 136.36 | 298.86 | 0.5006 | 1.0588 | 386.85 | 1.341 | 445.95 | 1.503 |
| 20 | 57.2905 | 0.0051 | 142.97 | 294.96 | 0.5221 | 1.0406 | 386.88 | 1.334 | 446.64 | 1.497 |
| 22 | 60.0308 | 0.0047 | 150.02 | 290.36 | 0.5449 | 1.0203 | 386.87 | 1.327 | 447.29 | 1.491 |
| 24 | 62.8773 | 0.0043 | 157.71 | 284.80 | 0.5695 | 0.9972 | 386.81 | 1.320 | 447.91 | 1.485 |
| 26 | 65.8368 | 0.0039 | 166.36 | 277.80 | 0.5971 | 0.9697 | 386.70 | 1.313 | 448.51 | 1.478 |
| 28 | 68.9182 | 0.0035 | 176.72 | 268.30 | 0.6301 | 0.9342 | 386.53 | 1.305 | 449.07 | 1.472 |
| 30 | 72.1369 | 0.0029 | 191.65 | 252.23 | 0.6778 | 0.8776 | 386.30 | 1.298 | 449.58 | 1.466 |
| 30.98 | 73.7730 | 0.0021 | 219.34 | 219.34 | 0.7680 | 0.7680 | 386.15 | 1.294 | 449.82 | 1.463 |

